# **DESIGN OF FLOOR SLAB**

#### Design Data

Dimensions of the slab (c/c distance b/w supports),

Length of short span,  $L_x = 4.00 \text{ m}$ 

Length of long span, = 5.30 m

Assume dia. of reinforcement steel

Width of the supporting beam, = 230mm Clear cover to main reinforcement = 20 mm

### **Calculations**

150 Assume the thickness of slab as mm; Effective depth, d = 125

Effective span,  $l_x = 4 \text{ m (or) } 3.895 \text{ m whichever is less;}$ d = 3.895

= 10

 $l_v = 5.3 \text{ m}$  (or) 5.195 m whichever is less; d = 5.195m

mm

 $(I_y/I_x) = 1.33 < 2$ ; Here,  $(I_y/I_x)$  is less than 2, Hence design the slab as two way slab

## **Load Calculations**

Dead Load of slab =  $0.15 \times 25$  $= 3.75 \text{ KN/m}^2$ 

Finishes load on slab  $= 2.00 \text{ KN/m}^2$ = 1.5 Live Load on slab KN/m<sup>2</sup>

Total Dead load acting on the Structure =  $5.75 \text{ KN/m}^2$ 

Total live load acting on the Structure = 1.5 KN/m<sup>2</sup> Factored Design Load w = 10.88KN/m<sup>2</sup>

**Support Condition** (Type of panel according to support condition)

One Short Edge Discontinuous

Short span coefficient for  $(I_v / I_x) =$ 1.33,

For negative moment, 0.0522

For positive moment,  $a_x =$ 0.0396 For this support condition,

N/mm<sup>2</sup>

N/mm<sup>2</sup>

Long span coefficient,

For negative moment, 0.037  $a_v =$ 0.028

For positive moment,

## **Moment Calculation**

Max. BM per unit width,  $M_x = a_x w I_x^2$ 

	$M_u$	$M_u / bd^2$	p <sub>t</sub>	$A_{st, req}$
	KNm	N/mm <sup>2</sup>	%	$mm^2$
For Short Span,				
At mid span,	6.54	0.42	0.1187	148
At supports,	8.62	0.55	0.1565	196
For Long span,				
At mid span,	4.62	0.35	0.0986	123
At supports,	6.11	0.46	0.1303	163

 $M_v = a_v w I_x^2$ 

 $A_{st, min} = (0.12/100) bD$  $mm^2$ 

#### Reinforcement details

Provide Y 8 @ 150 mm c/c at midspan & supports for short span  $(A_{st} pro. = 335 mm^2)$ Provide Y 8 150 mm c/c at midspan &  $(A_{st} pro. = 335 mm^2)$ supports for long span

#### Check for Deflection

Percentage of tension reinforcement = 0.27

 $f_s = 0.58 f_v (A_{st reg} / A_{st pro})$ = 128

Refer Fig. 4 of IS 456,

Modification factor = 1.41 Allowable (Span / d<sub>eff</sub> ) ratio = 36.7

Effective depth required = 106 mm

< d prov.

**Hence OK** 

