# **DESIGN OF FLOOR SLAB**

### Design Data

Dimensions of the slab (c/c distance b/w supports),

 $L_x = 5.3$ Length of short span,

Length of long span,

m

Width of the supporting beam, = 230 mm

Clear cover to main reinforcement = 20

mm Assume dia. of reinforcement steel = 10 mm

### **Calculations**

Assume the thickness of slab as 150 mm; Effective depth, d = 125

Effective span,  $l_x = 5.3 \text{ m}$  (or) 5.195 m whichever is less; d = 5.195m

 $l_v = 5.3 \text{ m}$  (or) 5.195 m whichever is less; d = 5.195m

 $(I_y/I_x) = 1.00 < 2$ ; Here,  $(I_y/I_x)$  is less than 2, Hence design the slab as two way slab

### **Load Calculations**

Dead Load of slab =  $0.15 \times 25$  $= 3.75 \text{ KN/m}^2$ 

Finishes load on slab  $= 2.00 \text{ KN/m}^2$ 

= 1.5 Live Load on slab KN/m<sup>2</sup>

Total Dead load acting on the Structure =  $5.75 \text{ KN/m}^2$ 

Total live load acting on the Structure = 1.5KN/m<sup>2</sup>

Factored Design Load w = 10.88KN/m<sup>2</sup>

#### **Support Condition** (Type of panel according to support condition)

Two Adjacent Edges Discontinuous

Short span coefficient for  $(I_v / I_x) =$ 

For negative moment,  $a_x = 0.0470$ 

For positive moment,  $a_x = 0.0350$  For this support condition,

N/mm<sup>2</sup>

N/mm<sup>2</sup>

Long span coefficient,

For negative moment, 0.047

0.035

For positive moment,  $a_v =$ 

## **Moment Calculation**

Max. BM per unit width,  $M_x = a_x w I_x^2$ 

		$M_u$	$M_u/bd^2$	$p_t$	$A_{st, req}$
		KNm	N/mm <sup>2</sup>	%	$mm^2$
For SI	nort Span,				
At mic	d span,	10.28	0.66	0.1888	236
At sup	ports,	13.80	0.88	0.2546	318
For Lo	ong span,				
At mic	d span,	10.28	0.78	0.2245	281

# $M_y = a_v w I_x^2$

 $A_{st, min} = (0.12/100) bD$ 180  $mm^2$ 

### Reinforcement details

Provide Y 10 @ 150 mm c/c at midspan & supports for short span  $(A_{st} pro. = 524 mm^2)$ Provide Y 10 150 mm c/c at midspan &  $(A_{st} pro. = 524 mm^2)$ supports for long span

## Check for Deflection

At supports,

% Percentage of tension reinforcement = 0.42

1.04

0.3035

13.80

 $f_s = 0.58 f_v (A_{st req} / A_{st pro})$ = 131

Refer Fig. 4 of IS 456,

Modification factor = 1.9

Allowable (Span / d<sub>eff</sub> ) ratio = 49.4

Effective depth required  $= 105 \, \text{mm}$ 

< d prov.

**Hence OK**